

**Amendments to the Drawings**

Applicants attach herewith as Appendix B a clean and a marked up version of replacement drawings sheets 1-11 to be entered into the application, incorporating matter from U.S. Application Serial No. 10/668,975, previously incorporated into the application by reference. The amendments to the drawings contain no new matter.

## **REMARKS/ ARGUMENTS**

The Final Office Action of June 16, 2006 has been carefully reviewed and this response addresses the Examiner's concerns.

### **I. STATUS OF THE CLAIMS**

Claims 1-10 are pending in the application. Claim 11 has been withdrawn.

Claim 1-5 are rejected under 35 U.S.C. 112, first paragraph, as being based on a disclosure, which is not enabling.

Claims 1-3 and 5-10 are rejected under 35 U.S.C. §102(e) as being anticipated by Stone (US 6,585,382).

### **II. SUPPORT FOR THE AMENDMENTS TO THE SPECIFICATION**

The material being inserted is the material previously incorporated by reference from U.S. Patent application Ser. No. 10/668,975 and from U.S. Patent 5,771,320 and the amendment contains no new matter.

### **III. SUPPORT FOR THE AMENDMENTS TO THE DRAWINGS**

The material being inserted is the material previously incorporated by reference from U.S. Patent application Ser. No. 10/668,975 and the amendment contains no new matter.

### **IV. THE 35 U.S.C. 112 REJECTION**

*Claim 1 is rejected under 35 U.S.C. 112, first paragraph, as being based on a disclosure, which is not enabling.*

After copying the material from U.S. Patent application Ser. No. 10/668,975, which was incorporated by reference,. Applicants state that Figs 4, 5, 6a and 6b of the substitute specification illustrate a “polarization separating sub-system being optically disposed to receive an input optical beam of arbitrary polarization and also being capable of separating the input optical beam into a first optical beam of a first polarization and a second optical beam of a second polarization, said second polarization being distinct from said first polarization, and emitting a first emitted optical beam of the first polarization and a second emitted optical beam of the first polarization, said emitted first and emitted second optical

beams constituting an input channel of the first polarization” and a “polarization recombining sub-system being optically disposed to receive the at least one transmitted optical beam of the first polarization and the at least one other transmitted optical beam of the first polarization and capable of recombining the at least one transmitted optical beam of the first polarization and the at least one other transmitted optical beam of the first polarization into at least one final output beam.”

Also Applicants respectfully state that Claim 1 is enabled by the “polarizing beam-splitter and a patterned polarization converter” of Paragraph 31 as well as by the substitute specification which incorporates the material from U.S. Patent application Ser. No. 10/668,975, filed on September 23, 2003, incorporated by reference..

Claims 2-5 are enabled in a similar manner.

Applicants have copied onto the substitute specification the relevant portions of U.S. Patent 5,771,320. However, regarding the incorporation by reference of U.S. Patent 5,771,320, Applicants respectfully restate 37 CFR 1.57(c), ““Essential material” may be incorporated by reference, but only by way of an incorporation by reference to a U.S. patent or U.S. patent application publication, which patent or patent application publication does not itself incorporate such essential material by reference.” Applicants also note that the same material is presented in original figures 2a, 2b, and 3, which would be inoperative if the second grating were a reflection grating (a switch mirror).

#### V. THE 35 U.S.C. §102 REJECTION

*Claims 1-3 and 5-10 are rejected under 35 U.S.C. §102(e) as being anticipated by Stone (US 6,585,382, the ‘382 patent).*

Although, as shown below, Applicants state that the ‘382 patent does not anticipate the Applicants’ claimed invention, a declaration by Applicant Stone is attached in which Applicant Stone states that any invention described in the ‘382 patent related to the invention claimed in the present application originated from Applicant Stone.

In order to demonstrate why the '382 patent does not anticipate the Applicants' claimed invention, Applicants compare the limitations of the claimed invention recited in claim 1 to the teachings of the 382 patent. The '382 patent teaches volume phase holographic switchable mirrors (the '382 patent, col. 3, line 2, line 5-6). Referring to Figure 1, these 382 patent states, in col. 4, lines 35-38, that "FIG. 1 of the drawings which depicts a plurality (three being illustrated therein) of switchable mirrors (or switchable mirror arrays, used interchangeably here) 12, 14, 16." Applicants respectfully state that the '382 patent does not teach "at least one switchable transmission diffraction grating."

The Examiner states in the Office Action that Stone teaches switchable mirrors and switchable gratings interchangeably. While the Applicants were unable to find that statement in the '382 patent (the '382 patent repeatably states that "the terms switched mirrors and switchable mirrors are used interchangeably throughout the application"), even if it were so, the statement does not imply that switchable mirrors are interchangeable in the present claimed invention with switchable transmission gratings. That in fact switchable mirror can not be interchanged for the claimed switchable transmission gratings can be seen from figures 1, 2a, 2b, and 3 of the original specification. In figure 1 of the original specification, if the grating were a volume phase holographic switchable mirror a variable attenuator would not be obtained since the output would be either 1 or zero. In figures 2a, 2b, and 3 of the original specification, if the second grating is a mirror, there would be no output at the system (furthermore, replacing what is stated to be in the reference a switchable mirror with a switchable transmission grating would render the prior art non-anticipatory.) Applicants respectfully state that claim 1 is not anticipated by the '382 patent.

Claim 2 recites "a static grating optically disposed between said at least one switchable transmission diffraction grating and said polarization recombining sub-system." The Examiner equates the static grating to that described in col. 6, lines 6-20 of these 382 patent. Col. 5, lines 66-67 and Col. 6, lines 6-20 of these 382 patent state

"In one of the preferred embodiments of the invention, volume phase holographic switchable mirrors are used to permit switching of the incident energy between the transmitted and reflected directions. Such switchable mirrors may be controlled by electrical switching, optical switching, and

polarization switching of the mirrors, as discussed with specific embodiments of the invention. Recently it has been demonstrated that high efficiency volume diffraction gratings which are recorded in permeable media, such as the DMP-128 photopolymer manufactured by Polaroid Corporation, Cambridge, Massachusetts can be made to be rapidly switchable between high and low diffraction efficiency states under electric control by imbining the structure with liquid crystals. In this technique, the crystals are rotated by the applied electric field and their refractive index switches in the range between ordinary and extraordinary values. By choosing the materials so that one of these switchable values of refractive index matches that of the phase modulation in the grating, the grating modulation is effectively switched "off-and-on" as the liquid crystal "fill" material index matches and mismatches the modulation, respectively “

As can be seen from the above, these 382 patent describes volume holographic mirrors which, as Examiner states, by maintaining a constant electric field, we produce a mirror not a static grating. The ‘382 patent does not teach “a static grating” and neither does it teach “a static grating optically disposed between said at least one switchable transmission diffraction grating and said polarization recombining sub-system.”

Applicants respectfully state that while a switchable diffraction grating may be a switchable reflective diffraction grating if it is designed to be so, that does not equate to a switchable reflective diffraction grating being interchangeable with a switchable transmission diffraction grating in the present claimed invention. Applicants respectfully state that such a difference can be seen from Samuel C. Barden, James A. Arns, and Willis S. Colbur, *Volume-phase holographic gratings and their potential for astronomical applications*, Proceedings SPIE vol. 3355, "Optical Astronomical Instrumentation" pp. 866-876, 1998, a copy of which is attached.

The Examiner states that "pixellated retarder" is interchangeable with a "steering grating." Applicants are unable to locate a reference to that interchangeability in U.S. 5,692,077. A retarder is defined as “device that uses nematic liquid crystals sandwiched between fused silica substrates to change the phase of polarized light. The cell is tunable from half-wave to

zero retardation because variation of the applied voltage results in different degrees of birefringence in the liquid crystal," according to the Photonics Dictionary available at <http://www.photonics.com/directory/dictionary/lookup.asp?url=lookup&entrynum=4561&letter=r> A steering grating, according to the preceding definition, is not a retarder. Applicants respectfully state that such an interchangeability is not found in U.S. 5,692,077 and would be contrary to accepted optical concepts.

Claim 4 as amended recites "a static grating optically disposed between said polarization separating sub-system and said at least one switchable transmission diffraction grating." The above statements related to static gratings also applied to claim 4.

Claims 2 through 7 are dependent claim 1 and since , as stated above, claim 1 is not anticipated by the 382 patent, claims 2-7 are not anticipated by the 382 patent.

Claim 5 as amended recites "two switchable transmission diffraction gratings" The '382 patent does not teach " two switchable transmission diffraction gratings." See Figs 13a, 13b of the '382 patent as well as col. 3, line 2, line 5-6, of the '382 patent.

The method of claim 8 also uses a static grating. Since as stated above, .The '382 patent does not teach "a static grating," claim 8 is not anticipated by the 382 patent.

Claims 9-10 depend on claim 8 and since claim 8 is not anticipated by the '382 patent, claims 9-10 are not anticipated by the 382 patent.

**To anticipate a claim a reference must teach every element of the claim.** (MPEP § 2131). "A claim is anticipated only if each and every element as set forth in the claim is found, either expressly or inherently described, in a single prior art reference." *Verdegaal Bros. v. Union Oil Co. of California*, 814 F.2d 628, 631, 2 USPQ2d 1051, 1053 (Fed. Cir. 1987).

As stated above, the '382 patent does not teach all the elements of Claims 1-5 or 5-10. Applicants respectfully state that claims 1-5 and 5-10 are not anticipated by the '382 patent.

VI. CONCLUSION

In conclusion, in view of the above remarks, Applicants respectfully request the Examiner find claims 1-10 allowable over the prior art and pass this case to issue.

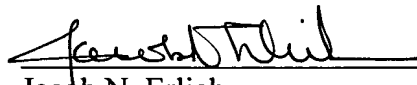
No additional fees are believed to be required for the consideration of this response. However, if fees are required, they should be charged to Deposit Account No. 50-3718.

In accordance with Section 714.01 of the MPEP, the following information is presented in the event that a call may be deemed desirable by the Examiner:

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Respectfully submitted,  
Thomas W. Stone et al., Applicants

Dated: August 16, 2006

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01042750

# Volume-phase holographic gratings and their potential for astronomical applications

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## ABSTRACT

A diffraction grating technology based upon volume-phase holograms shows promise of enhanced performance for many applications in astronomical spectroscopy over classical surface-relief grating technology. We present a discussion of the underlying physics of a volume-phase grating, give some theoretical performance characteristics, present performance data for a real volume-phase grating, and discuss some potential applications for this grating technology.

Keywords: diffraction gratings, holographic gratings, spectrographs, astronomical instruments

## 1. INTRODUCTION

In recent years, a new type of grating has been developed using holographic techniques<sup>1</sup>. Rather than being diffracted by surface-relief structures as in a surface grating (generated either by diamond ruling or by a holographic exposure of a photoresist layer), the light undergoes Bragg diffraction as it passes through the volume of a thin layer in which the refractive index is modulated. These volume-phase (VP) holographic gratings show promise for improved performance over classical, low-order, surface-relief gratings in the following areas:

- The "blaze" or efficiency envelope is governed by Bragg diffraction and can be tuned by adjustment of the grating angle for different wavelengths or diffraction orders.
- They can have high diffraction efficiencies approaching 100% for high line density (600 to 6000 l/mm), high dispersion transmission gratings with relatively low dependence on polarization angle.
- The technology can likely produce very large grating sizes (at least 600 by 850 mm).
- Complex grating structures can be produced to minimize optical elements in some spectrograph configurations, simplifying spectrograph design and enhancing spectrograph efficiency.
- The grating is sandwiched between two substrates providing an environmentally stable device which is robust, can be cleaned, can have anti-reflection coatings applied, and is capable of long lifetimes without degradation.
- Grating customization is relatively straightforward as each grating is an original rather than a replica of an expensively ruled master.
- Both transmission and reflection grating geometries are possible.

VP grating technology can improve both the versatility and the efficiency of optical astronomical spectrographs.

A brief overview of the underlying physics is presented and followed by a discussion of both theoretical and actual grating performance. We close with a discussion on many of the various possibilities provided by volume-phase gratings.

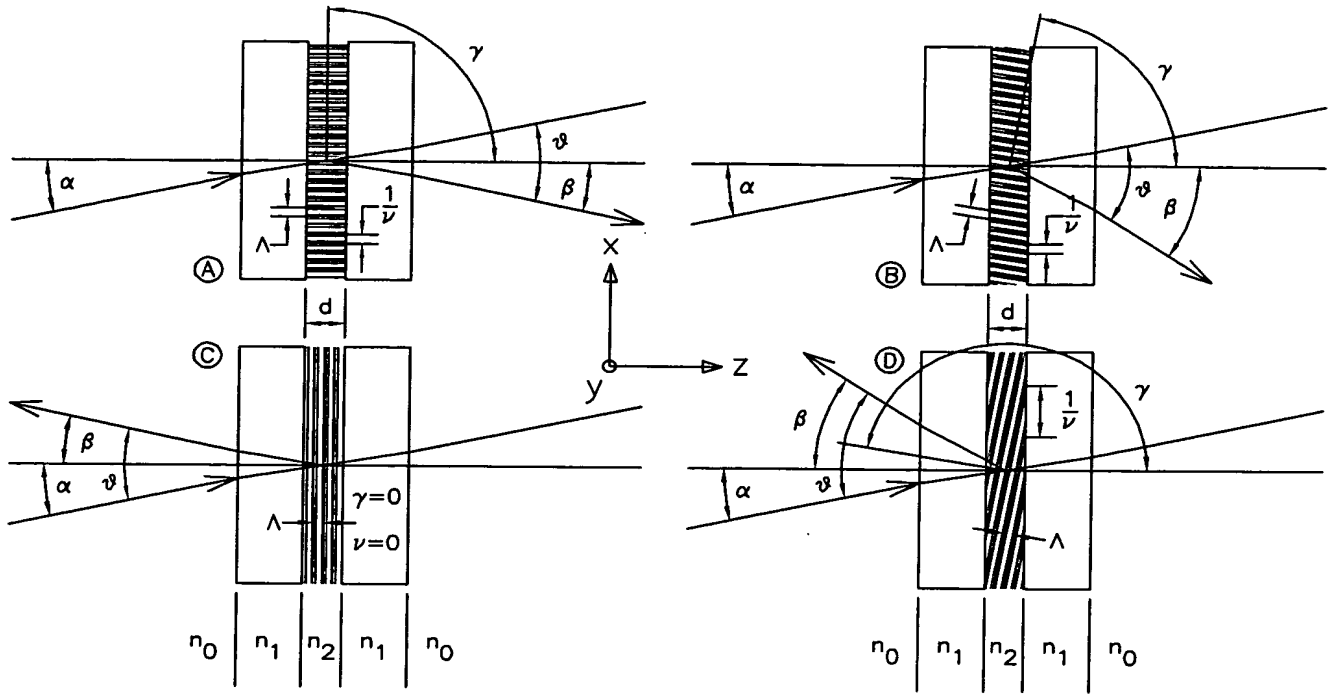
## 2. VOLUME-PHASE GRATING PHYSICS

The diffracting mechanism in VP gratings arises from modulations in the refractive index in the form of fringe planes running parallel to each other through the depth of the grating material and oriented so that the fringes terminate at the surfaces of the volume<sup>2,3</sup>. Figure 1 schematically displays the structure and geometry of four types of VP gratings.

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\* Operated by the Association of Universities for Research in Astronomy, Inc. (AURA) under cooperative agreement with the National Science Foundation.





**Figure 1.** Some possible VP grating configurations showing Bragg condition diffraction. **A.** Transmission grating with fringes perpendicular ( $\gamma = 90$  degrees) to the grating surface (unslanted fringes). In this case the magnitude of  $\alpha$  equals that of  $\beta$  for the Bragg condition. **B.** Transmission grating with tilted fringes. **C.** Reflection grating with fringes parallel ( $\gamma = 0$ ) to the grating surface. This grating does not disperse the light since  $v$  is zero. Again, the magnitude of  $\alpha$  and  $\beta$  are equivalent for the Bragg condition. **D.** Reflection grating with tilted fringes.

The spacing ( $1/v$ ) of the fringe planes as they intersect the surface of a VP grating define the grating dispersion, diffracting light according to the standard grating equation in the same manner as a classical surface-relief grating. The grating equation for a transmissive VP grating can be represented by

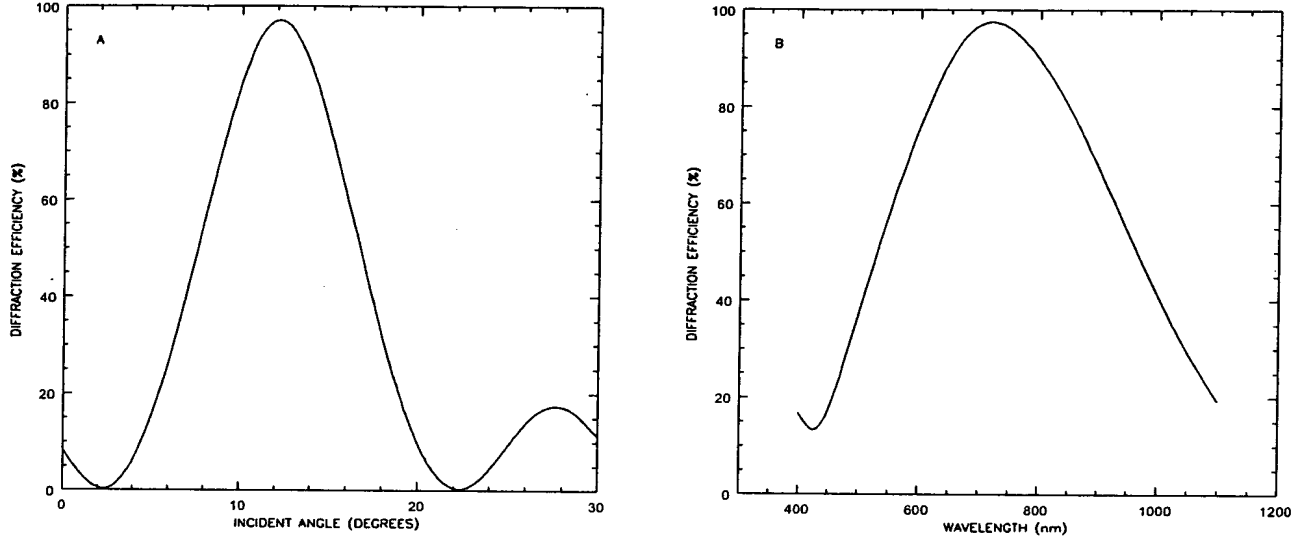
$$mv\lambda = \sin(\alpha) - \sin(\beta) \quad (1)$$

where  $m$  is the order of diffraction,  $v$  is the grating frequency,  $\lambda$  is the wavelength of light in free space,  $\alpha$  is the angle of incidence in air, and  $\beta$  is the angle of diffraction in air. Light traversing a VP grating, however, is also affected by interaction with the fringes as it travels through the bulk or volume of the grating material. The depth of the grating volume, the intensity or contrast of the fringe structure, and the angular and spectral relationship of the incident light to the Bragg condition determine how much light goes into which order. The Bragg condition for a plane, parallel grating with fringes that are normal to the grating surface (the case shown in Figure 1a) is given by

$$m\lambda = \Lambda 2 n_2 \sin(\alpha_{2B}) \quad (2)$$

where  $\Lambda$  is the fringe spacing of the grating equal to  $1/v$  for fringe planes orthogonal to the grating surface, and  $\alpha_{2B}$  is the Bragg angle in the grating medium. The Bragg condition is met when  $m$  is an integer and the wavelength and fringe spacing are such that the angles of incidence and diffraction are equal and opposite (with respect to the surface normal). The formulation of the Bragg condition for slanted fringes is slightly more complex, but in that case the angles of incidence and diffraction are symmetric within the grating medium about the fringe planes. Light illuminating the grating at angles significantly outside of the Bragg condition may pass through the grating without being diffracted. However, near the angle at which the Bragg condition is satisfied there is a range of angles for which light will still be efficiently diffracted; these

angles can be thought of as falling within a Bragg envelope and having an angular bandwidth as shown by the sample curve in Figure 2a. Similarly, the wavelength that satisfies the Bragg condition is called the Bragg wavelength, and again there is a Bragg envelope of wavelengths about the Bragg wavelength that are diffracted efficiently as shown in Figure 2b. Wavelengths that are significantly outside the spectral bandwidth may pass through the grating undiffracted. It is this selective aspect which allows these gratings to be tuned for different orders of diffraction and or wavelengths by tilting the grating with respect to the incident beam of light.



**Figure 2.** The angular and wavelength bandwidth Bragg envelopes for a theoretical 600 l/mm grating designed for 1<sup>st</sup> order operation at 700 nm. *A. Angular bandwidth Bragg envelope. B. Wavelength bandwidth Bragg envelope.*

Figure 1 shows the grating parameters ( $\alpha, \beta, \gamma, \theta, \Lambda, d, n_2$ ) which, along with the amplitude of the index of refraction modulation ( $\Delta n_2$ ), determine the grating performance. The index of refraction,  $n_2$ , for the grating itself is the average value of the modulated refractive index,  $n_2(x,z)$ , and is approximately represented by

$$n_2(x,z) = n_2 + \Delta n_2 \cos[(2\pi/\Lambda)(x \sin(\gamma) + z \cos(\gamma))] \quad (3)$$

for the case of either slanted or unslanted fringes where  $\Delta n_2$  is the semi-amplitude of the variation in the index of refraction within the grating volume. The substrate index of refraction is given by  $n_1$  and the refractive index for air is  $n_0$  (assumed to be equal to 1).

Volume-phase gratings can be analyzed by means of either a rigorous coupled-wave analysis<sup>4,5</sup> or a modal analysis<sup>6</sup>; the two approaches are exact and can be shown to be equivalent<sup>7</sup>. In their most rigorous forms, these approaches require computer-derived solutions. Using a simplified coupled-wave analysis that includes only zeroth and first order diffraction, Kogelnik<sup>8</sup> developed a set of closed-form equations that are sufficiently accurate in many cases, and that are widely used in the field of volume holography.

The diffraction efficiency, spectral bandwidth, and angular bandwidth are influenced by the Bragg condition and are functions of the intensity of the grating modulations ( $\Delta n_2$ ) and the thickness ( $d$ ) of the grating volume<sup>4,5,8</sup>. In general, a VP grating with a wide spectral bandpass has a lower peak diffraction efficiency than a grating with a narrower bandpass. For transmission gratings, the peak diffraction efficiency at the Bragg condition is a function of both the grating thickness and modulation intensity. For orthogonal fringe (unslanted) plane gratings the efficiency  $\eta$  at the 1<sup>st</sup> order Bragg condition is<sup>8</sup>

$$\eta = \sin^2[\pi \Delta n_2 d / (\lambda \cos(\alpha_{2B}))] \quad (4)$$

where  $\alpha_{2B}$  is the angle within the grating material (where  $n = n_2$ ) given by the relation

$$\sin(\alpha_{2B}) = (n_0 / n_2) \sin(\alpha). \quad (5)$$

The 1<sup>st</sup> order spectral bandwidth and angular bandwidth for unslanted, transmission gratings are approximated by<sup>8</sup>

$$\Delta\lambda_{FWHM} / \lambda \sim (\Lambda/d) \cot(\alpha_{2B}), \quad (6)$$

$$\Delta\alpha_{FWHM} \sim \Lambda/d \quad (7)$$

where  $\Delta\alpha_{FWHM}$  is in radians. The challenge in VP grating fabrication is to produce a grating with appropriate thickness and refractive index modulation to provide the desired peak efficiency and bandwidth performance.

Polarization dependence in VP gratings is dominated by a reduced coupling constant for parallel polarization of light with respect to the plane of incidence (p or TM polarization)<sup>8</sup>, whereby Equation (4) becomes

$$\eta = \sin^2 \{ [\pi \Delta n_2 d / (\lambda \cos(\alpha_{2B}))] \cos(\theta_2) \} \quad (8)$$

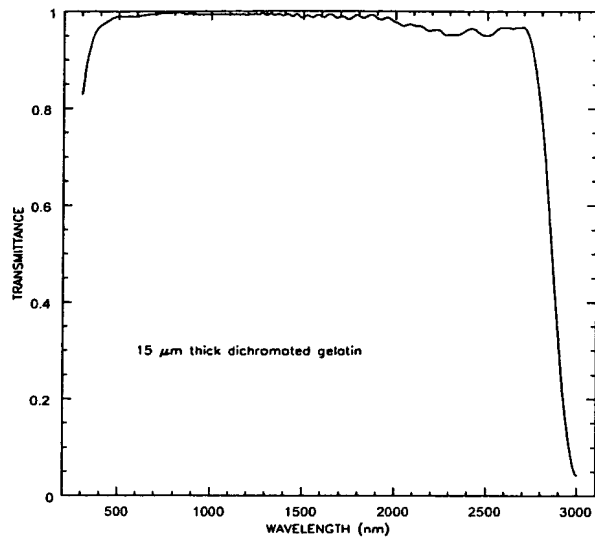
where  $\theta_2$  is the angle within the medium between the incident ( $\alpha_{2B}$ ) and diffracted ( $\beta_2$ ) wavefronts. When the angle between the incident and diffracted waves within the grating equals 90°, the diffraction efficiency for this polarization state goes to zero. Polarization dependencies can be minimized as long as this condition is avoided.

### 3. GRATING FABRICATION

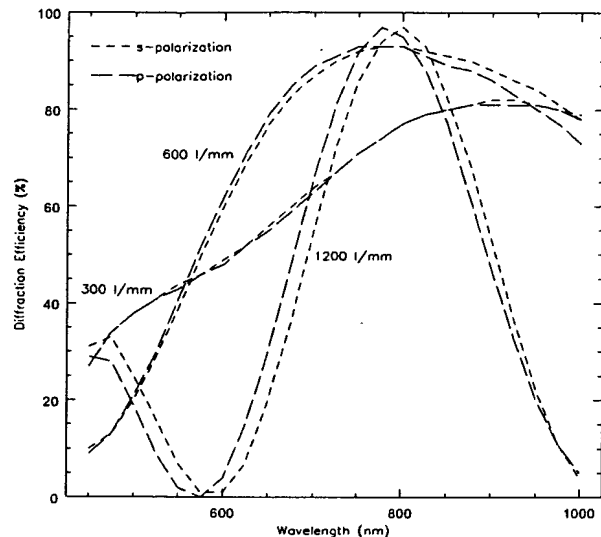
The VP gratings in this study are fabricated in dichromated gelatin. A thin film of sensitized gelatin is deposited onto a glass substrate and exposed in a holographic exposure system to record an interferometrically produced wave pattern of the desired fringe frequency and orientation. Wet processing transforms the exposed fringes into refractive index modulations within the gelatin. Once the desired grating parameters have been achieved, a cover glass is laminated over the gelatin surface. The substrate may be any glass material; typical optical glasses used are BK7 and fused silica. Anti-reflection coatings can be applied to the substrates to reduce reflection losses. It is also possible to use prisms and plano-convex or plano-concave lenses in the grating assembly.

Contrary to the statement that dichromated gelatin “is not an attractive candidate for high accuracy, because it is difficult to process gelatin in such a way that the modulation pattern is accurately reproduced after a wet-dry processing cycle”<sup>9</sup>, this material has been used extensively in holographic components for over twenty five years with a proven record of producing high quality diffraction elements with high diffraction efficiency, high clarity, low scatter, low absorption, and long lifetime when properly treated in the fabrication process and adequately protected against degrading environmental conditions<sup>10,11,12</sup>. Due to the hygroscopic nature of the gelatin, a protective cover glass is required to prevent water vapor from affecting the sensitive film and to protect the grating from contaminants. Properly sealed dichromated gelatin holograms can have lifetimes of at least 20 years if they are given reasonable care and handling. Their application as head-up display components in military aircraft show that elements fabricated in this manner can withstand considerable humidity and temperature extremes.

Figure 3 shows the transmission behavior of dichromated gelatin between 300 and 3000 nm. It is apparent that the material may have a useful spectral range from 300 nm to 2.8  $\mu\text{m}$ . VP gratings are currently and routinely fabricated for use between 400 nm and 1.5  $\mu\text{m}$ . Typical values of  $n_2$ ,  $\Delta n_2$ , and  $d$  obtained with dichromated gelatin gratings are 1.5, 0.02 to 0.10, and 4 to 20  $\mu\text{m}$ , respectively. Line densities ( $\nu$ ) range from 300 to 6000 l/mm.



**Figure 3.** The transmittance as a function of wavelength for a 15  $\mu\text{m}$  thick layer of uniformly exposed and processed dichromated gelatin.



**Figure 4.** Rigorous coupled-wave prediction for the diffraction efficiency of three different gratings designed for first order operation at 790 nm. Both s and p polarization states are shown. Material and reflection losses are not included.

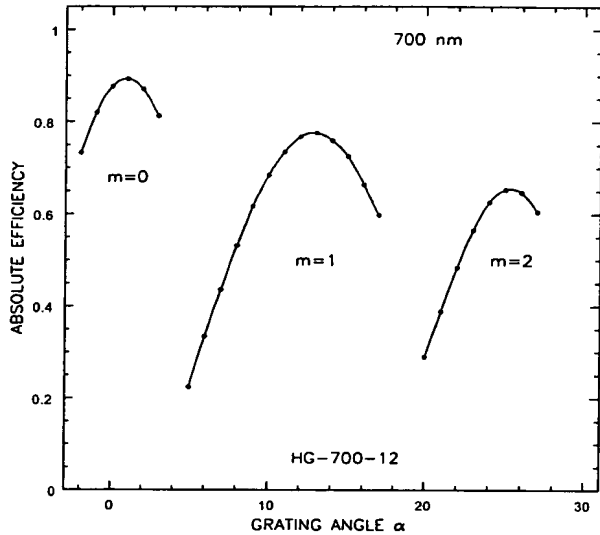
#### 4. GRATING PERFORMANCE

The high diffraction efficiency of dichromated gelatin and the characteristics of Bragg diffraction give the potential for very high efficiency dispersers. Figure 4 shows the theoretically achievable diffraction efficiencies derived through rigorous coupled-wave analysis<sup>4</sup> of three different transmissive VP gratings designed for operation at 790 nm. Notice that the peak diffraction efficiency and bandwidth are traded off against each other. Polarization effects are not very significant. For comparison, a reflective, surface-relief grating blazed at 790 nm will only have a theoretical peak efficiency of about 80% in unpolarized light due to the major dependency of efficiency on the angle of polarization<sup>9</sup>.

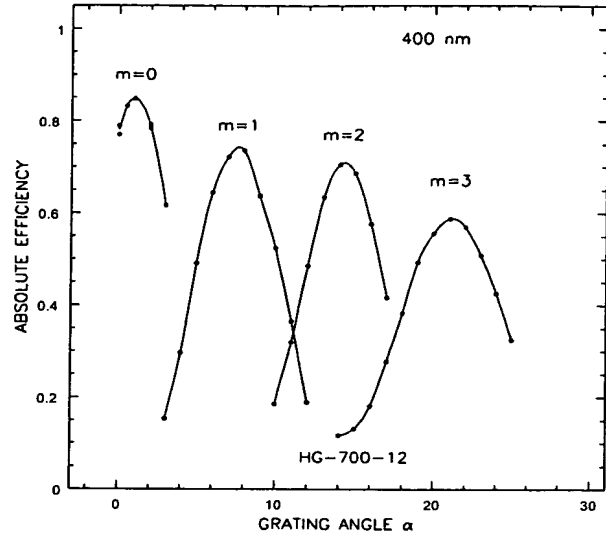
A 600 l/mm VP grating (HG-700-12) was produced by Kaiser Optical Systems, Inc. (KOSI) for evaluation at the National Optical Astronomy Observatories (NOAO) as part of an effort to design a new technology, high efficiency spectrograph. The grating was designed for optimal efficiency at 700 nm with a bandwidth covering the spectral region spanning 500 to 900 nm in the first order of diffraction. Peak efficiency was specified at 70 to 80% with greater than 50% efficiency at 500 and 900 nm. The grating modulations are perpendicular to the surface of the grating substrate, so the Bragg condition is met when the incident and diffracted angles are the same magnitude.

The absolute efficiency for unpolarized light was measured at NOAO at 400, 500, 633, 700, 800, and 900 nm as a function of incident angle and of diffracted angle. When the grating is illuminated at zero degrees incidence, the majority of the light passes undiffracted into the zeroth order. As the angle of incidence is increased, the level of diffraction increases. Peak diffraction into first order at 700 nm is achieved when the incident angle is about 12 degrees (the first order Bragg condition). At an angle of incidence equal to about 25 degrees, 700 nm meets the Bragg condition for second order diffraction. Figure 5 displays the absolute efficiency of the unpolarized light transmitted and diffracted by the grating at a wavelength of 700 nm as a function of angle of incidence and order of diffraction. A peak efficiency of nearly 80% is achieved for first order diffraction. In comparison with a comparable theoretical VP grating (see Figure 4), this grating is about 10% lower than might be expected. This is attributable to the inclusion of reflective and other material losses in the

measurements of Figure 5 and due to some residual uncertainty in the holographic process which optimizes the grating thickness and the index modulation. Future process refinements will lead to an improved capability of producing gratings with efficiencies that more closely approach the theoretical limits.



**Figure 5.** Absolute efficiency of the 600 l/mm VP grating for unpolarized light as a function of incident angle and diffracted order ( $m=0,1,2$ ) for 700 nm. Material and reflective losses are included.



**Figure 6.** Absolute efficiency of the 600 l/mm VP grating in unpolarized light at 400 nm for diffraction orders  $m=0, 1, 2$ , and 3. Material and reflective losses are included.

Comparable surface-relief gratings in use at Kitt Peak National Observatory (KPNO) give 70% efficiency at 700 nm in first order (Bausch and Lomb grating 420, 600 l/mm blazed at 750 nm) and 42% for 700 nm in 2<sup>nd</sup> order (Bausch and Lomb grating 450, 632 l/mm blazed at 1100 nm in 1<sup>st</sup> order and which has a peak efficiency in 2<sup>nd</sup> order of 50% at 550 nm). The VP grating shows good performance at the design wavelength in comparison with these other gratings. It also shows superior performance for the 2<sup>nd</sup> order of diffraction, a region in which it was not specifically designed to function!

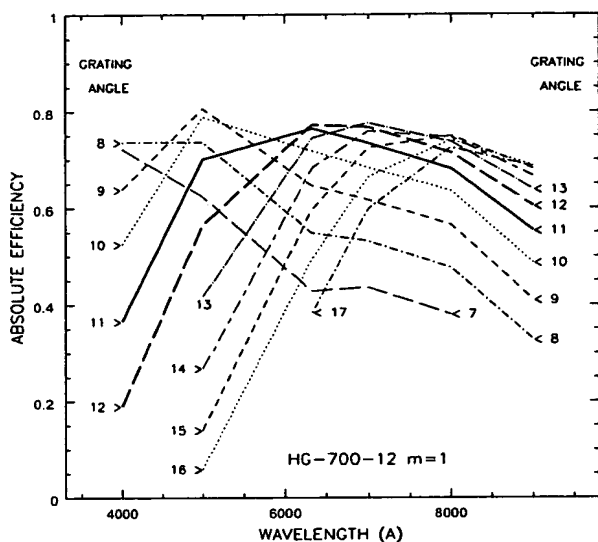
At 400 nm, the VP grating still shows excellent performance when aligned for Bragg diffraction at that wavelength for 1<sup>st</sup>, 2<sup>nd</sup>, and 3<sup>rd</sup> order diffraction (7, 14.2, and 21.6 degrees respectively). Figure 6 displays the measured absolute efficiencies for diffraction at 400 nm.

Comparable surface gratings at KPNO are inferior to this grating with only 50% efficiency for 1<sup>st</sup> order diffraction by a grating originally ruled at KPNO (KPC007, 632 l/mm blazed at 520 nm), 55% efficiency for 2<sup>nd</sup> order diffraction by another grating ruled at KPNO (KPC22b, 632 l/mm blazed at 850 nm in 1<sup>st</sup> order), and 40% in 2<sup>nd</sup> order by a Bausch and Lomb grating (Bausch and Lomb 450, 632 l/mm, blazed at 1100 nm in 1<sup>st</sup> order). The 3<sup>rd</sup> order diffraction efficiencies for any of the gratings at KPNO were unavailable for comparison.

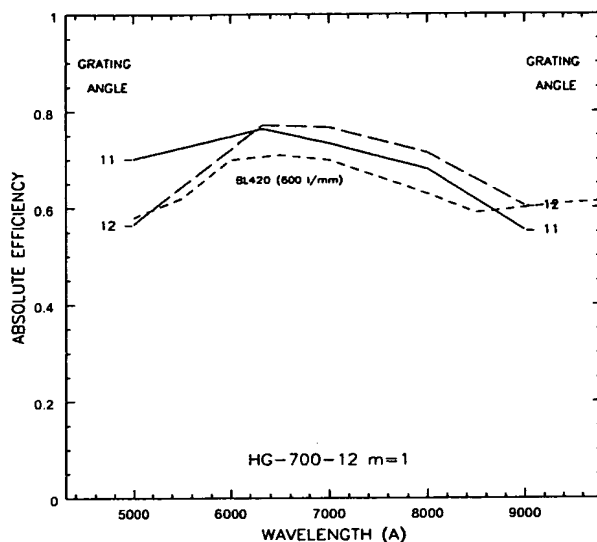
The strong performance in higher orders of diffraction for this grating is intriguing and has prompted the authors to further explore the feasibility of high order diffraction VP gratings. Very little research has been conducted in this area since the typical customer for volume holographic devices does not want high order diffraction. As a result, little or no effort has been expended to optimize the performance of a high order VP grating.

The bandwidth of the grating was determined by measuring the efficiency for each wavelength at a specific grating angle, or angle of incidence. Figure 7 shows the equivalent of the "blaze" function as a function of grating tilt for 1<sup>st</sup> order

diffraction. Tilts of 11 to 12 degrees give the best overall efficiency across the design spectral range of 500 to 900 nm with greater than 55% efficiency and a peak efficiency of nearly 80% between 600 and 700 nm. Note that the grating also makes an excellent, 1<sup>st</sup> order, blue grating when used at a grating tilt of 8 to 10 degrees. Comparison with the Bausch and Lomb 420 grating (600 l/mm, blazed at 800 nm) at KPNO (Figure 8) shows that the VP grating is about 5 to 10% more efficient across the entire design spectral range.

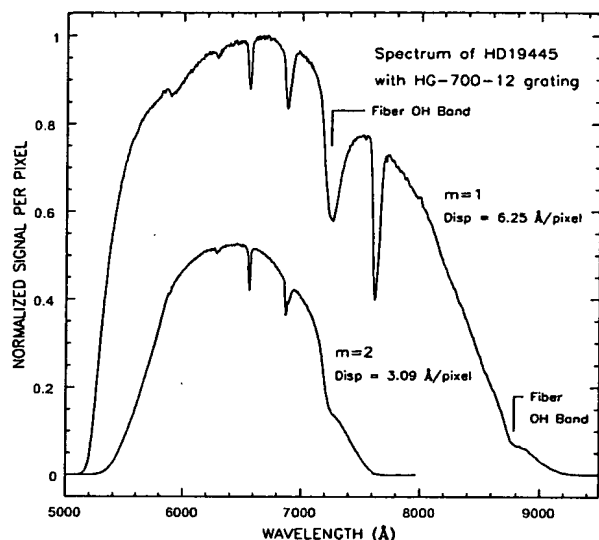


**Figure 7.** Efficiency envelope of the 600 l/mm VP grating as a function of incident angle for first order diffraction. Grating tilts of 11 and 12 degrees give the best overall efficiency in the design bandwidth from 500 to 900 nm.



**Figure 8.** Comparison of the 600 l/mm VP grating at grating tilts of 11 and 12 degrees to a diamond ruled, 600 l/mm, reflection grating blazed at 800 nm (Bausch and Lomb 420).

A simple, on-sky test was made with the test VP grating at the KPNO 2.1 meter telescope using a fiber optic feed onto an optical bench. The 22 meter long, 200  $\mu$ m diameter fiber optic cable fed light from the telescope to a 40 mm diameter achromatic doublet collimating lens. An OG515 high-pass filter was used to filter out 2<sup>nd</sup> order contamination. A second 40 mm diameter achromatic doublet lens was used to image the light dispersed by the test grating onto a 2048 Tektronix CCD binned 2 by 2 to get 48  $\mu$ m pixels. The system was first aligned at 12 degrees for first order diffraction from the grating. A standard star was observed and the count rate transformed into a flux rate. The total system (telescope, fiber aperture, fiber, lenses, grating, and detector) efficiency at 670 nm was measured to be 17.0%. The system was then reconfigured to 25 degrees for 2<sup>nd</sup> order diffraction at the same wavelength and another spectrum obtained. System efficiency was again measured to be 17.2% for 2<sup>nd</sup> order. Independent determination of the fiber, telescope, aperture, and detector efficiency showed that the two lenses plus grating were 60% efficient in the R band (144 nm bandwidth at 647 nm) in the first order of diffraction. This agrees remarkably well with the laboratory measurements especially given the uncertainty in the atmospheric seeing which was estimated to be variable by about 30% during the course of the observations. Figure 9 displays the spectra for both 1<sup>st</sup> and 2<sup>nd</sup> order configurations. Note that the shape of the spectra are dominated by the cutoff filter at 515 nm and by vignetting of the dispersed spectrum by the imaging lens (most notable in the 2<sup>nd</sup> order spectrum) along with the diminishing quantum efficiency of the CCD detector in the red portion of the spectrum.



**Figure 9.** *Stellar spectra obtained in first and second orders of diffraction. The units of the ordinate axis were selected to remove confusion of the two curves but give the false impression that the 2<sup>nd</sup> order spectrum has a factor of two lower signal.*

## 5.2 Reflection gratings

As shown in Figure 1, a reflection VP grating can be produced by creating a sufficient tilt in the holographic fringes with respect to the surfaces of the grating. The peak diffraction efficiency of a reflective VP grating can be quite high but in many cases the bandwidth may be narrower than desired. Some studies have shown that the bandwidth can be increased by modifications in the hologram processing<sup>14,15</sup>.

Most reflective VP holographic devices are currently designed to be non-dispersive. There appears to be little activity in the study or production of reflective VP gratings which disperse light into diffraction orders other than zero. Further study of dispersive reflective gratings, however, is warranted and desired. Other than potentially superior performance, the development of large, reflective VP gratings will allow drop-in replacements for many current astronomical spectrographs utilizing reflective surface-relief gratings.

## 5.3 Grating customization

One of the most frustrating aspects of currently available gratings is the lack of a sufficient sampling in the parameter space of peak efficiency and dispersion, especially with regards to large, astronomical gratings. In order to acquire a grating of desired properties, one must compromise to the closest available catalog grating or have a master grating generated. Quite often, the closest available grating is poorly matched to what is actually desired and large, custom, master, surface-relief gratings are expensive and take a considerable amount of time to generate.

VP holographic gratings are typically not replicas (though there are processes which could replicate VP gratings from a single master<sup>13</sup>) and are relatively straightforward to produce. As such, customization of the grating parameters is more easily attained without a major expenditure in cost or time.

# 5. POSSIBILITIES

## 5.1 Transmission gratings

The blazing for surface-relief, transmission gratings, particularly in the red portion of the optical spectrum, can be difficult and sometimes impossible due to the large facet angles and grating depths required. This is particularly true for high dispersion gratings (rulings greater than 600 l/mm for unimmersed gratings)<sup>9</sup>. Inclusion of a prism, making the grating into a grism, allows surface rulings of up to 1200 l/mm before production gets difficult. Many of these restrictions in performance arise from the presence of the surface facets that make the grating. Total internal reflection becomes an issue in the production of such gratings as well as complications in the ability to replicate a surface grating with large and steep grooves.

VP gratings are not limited by either total internal reflection on steep grooves or by the inability to replicate a grating with deep grooves since the grating mechanism arises from refractive index modulations rather than surface discontinuities. As such, VP gratings can be fabricated as transmission gratings with line densities of up to and greater than 6000 l/mm. The peak efficiency of a transmission VP grating can also exceed the peak limits of a transmissive surface-relief grating as a consequence of the different diffraction mechanism.

#### 5.4 Complex grating structures

The holographic nature of these gratings allows the stacking of holograms to make a variety of complex grating structures<sup>16,17</sup>. A single grating assembly might contain a second grating with the fringes perpendicular to the first in order to provide cross-dispersion. A second concept is a double grating which disperses light of two different wavelengths into the same angle of diffraction. For example, it would be possible to create a complex grating in which  $H\alpha$  light meets the Bragg condition of the first hologram but not the second and  $H\beta$  light satisfies the Bragg condition of the second but not the first VP grating. The correct ratio of line densities in the two gratings would direct both  $H\alpha$  and  $H\beta$  into the same angle of diffraction for simultaneous detection by a single detector. A third concept would be a dual grating that divides the light at different wavelengths into different paths to function as a dispersive beam splitter.

#### 5.5 Large gratings

VP gratings are currently fabricated by KOSI and utilized in their line of Raman spectrographs<sup>18</sup>. Although they currently only fabricate gratings of up to 75 by 100 mm in size, their facility can easily accommodate an upgrade for the production of gratings with dimensions of 200 by 280 mm. It is their desire to implement such an upgrade in the very near future. This would allow this interesting and valuable technology to be implemented in astronomical instruments on moderately large telescopes.

With the advent of 8 and 10 meter class telescopes, even gratings of 200 mm in size are becoming too small. The demand is increasing for gratings with sizes of 300 to 400 mm. Classical surface gratings are difficult and expensive to produce due to the wear of the diamond as the grating is ruled. Grating mosaics are possible (e.g. the Echelle grating in HIRES on Keck has 3 gratings to form a 300 by 1200 mm mosaic<sup>19</sup>), but complicated and also costly. State-of-the-art holographic exposure and processing technology is at a level where the production of very large VP gratings could be possible (greater than 600 mm). Indeed, holographically generated surface-relief gratings are already achieving rather large dimensions.

#### 5.6 Wavelength regime

KOSI currently fabricates gratings used in the visible and has recently started producing gratings for use at 1.5  $\mu\text{m}$ . There has not yet been any effort to produce a VP diffraction grating further towards the infrared. Future efforts may attempt to exploit the transmittance of dichromated gelatin out to 2.8  $\mu\text{m}$ . Behavior of dichromated gelatin at cryogenic temperatures would also need some study.

#### 5.7 Line density and diffraction angle

Gratings are currently fabricated with line densities between 300 and 6000 l/mm. Gratings with diffraction angles of up to 72 degrees have been produced at KOSI. Such high diffraction angle gratings are typically immersed to minimize reflection losses on the air-to-glass substrate surfaces.

#### 5.8 Immersed gratings

Immersion of a classical surface grating is another approach for achieving high resolution with a relatively small grating<sup>20</sup> but is difficult due to the fragile nature of the ruled surface. VP gratings, by their nature, are easily immersed.

#### 5.9 High order diffraction gratings

Little study has been expended on the performance of VP gratings at diffraction orders other than zeroth or first. What has been published<sup>21,22,23</sup> and the behavior of the NOAO test grating suggest that it may be possible to fabricate a relatively high order diffraction VP grating. An Echelle-like VP grating could possibly provide greater dispersing power over classical Echelles, especially given the simplicity of immersing a VP grating. Limitations for very high order gratings ( $m > 3$ ) may, however, arise from the inability of current holographic materials to achieve the required refractive index modulation for efficient diffraction into those high orders. Further theoretical and empirical study is needed.

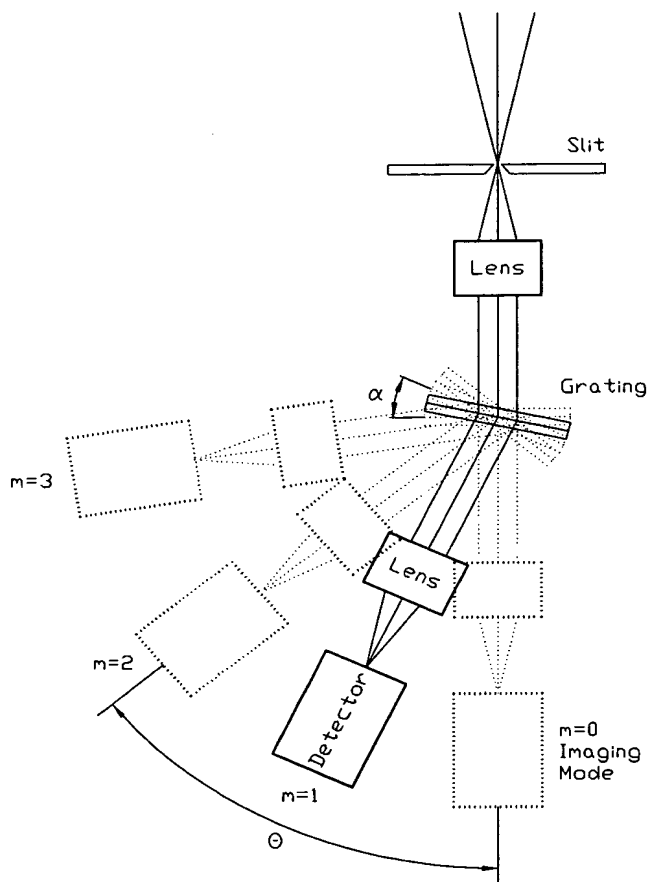
#### 5.10 Aberration correction gratings

Non-dispersive, VP holograms are currently used in military head-up display combiners that incorporate aberration correction within the hologram itself. Similar aberration correction can likely be incorporated into VP holographic gratings<sup>24</sup> in a similar fashion to current, concave, holographic, surface-relief gratings.



### 5.11 Tunable spectrographs

The nature of the test VP grating raises the possibility that a single grating can have a range of performance characteristics depending on the configuration of the spectrograph in which it is used. Such versatility from a single grating is not available with surface-relief gratings. With VP grating technology, it is possible to think of a spectrograph in which the peak efficiency and dispersive power can be tuned to the desired wavelength of interest with a simple change in both the grating angle and the angle between the collimator and the camera (see Figure 10). Although some complexity is added to the spectrograph housing, the need for separate gratings is eliminated or minimized. A simple, fiber-fed, bench-mounted spectrograph could easily accommodate these adjustments, making the instrument much more versatile than a spectrograph with a classical surface grating.



**Figure 10.** Schematic of a tunable spectrograph concept in which the camera axis angle ( $\theta$ ) and grating angle ( $\alpha$ ) are allowed to tilt in order to change the order of diffraction or to peak up the efficiency of the desired wavelength.

## 6. CONCLUSIONS

Volume-phase holographic gratings diffract light through a mechanism that is somewhat different from surface-relief grating structures. With VP gratings, one can achieve higher diffraction efficiencies, higher dispersion for transmissive gratings, and a range of versatility that is not possible with surface-relief gratings. Eventual utilization of this technology into astronomical spectrographs will enhance, complement, and possibly replace the suite of spectroscopic facilities currently in use.

## 7. ACKNOWLEDGEMENTS

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## **Appendix B**



1/11  
1/8

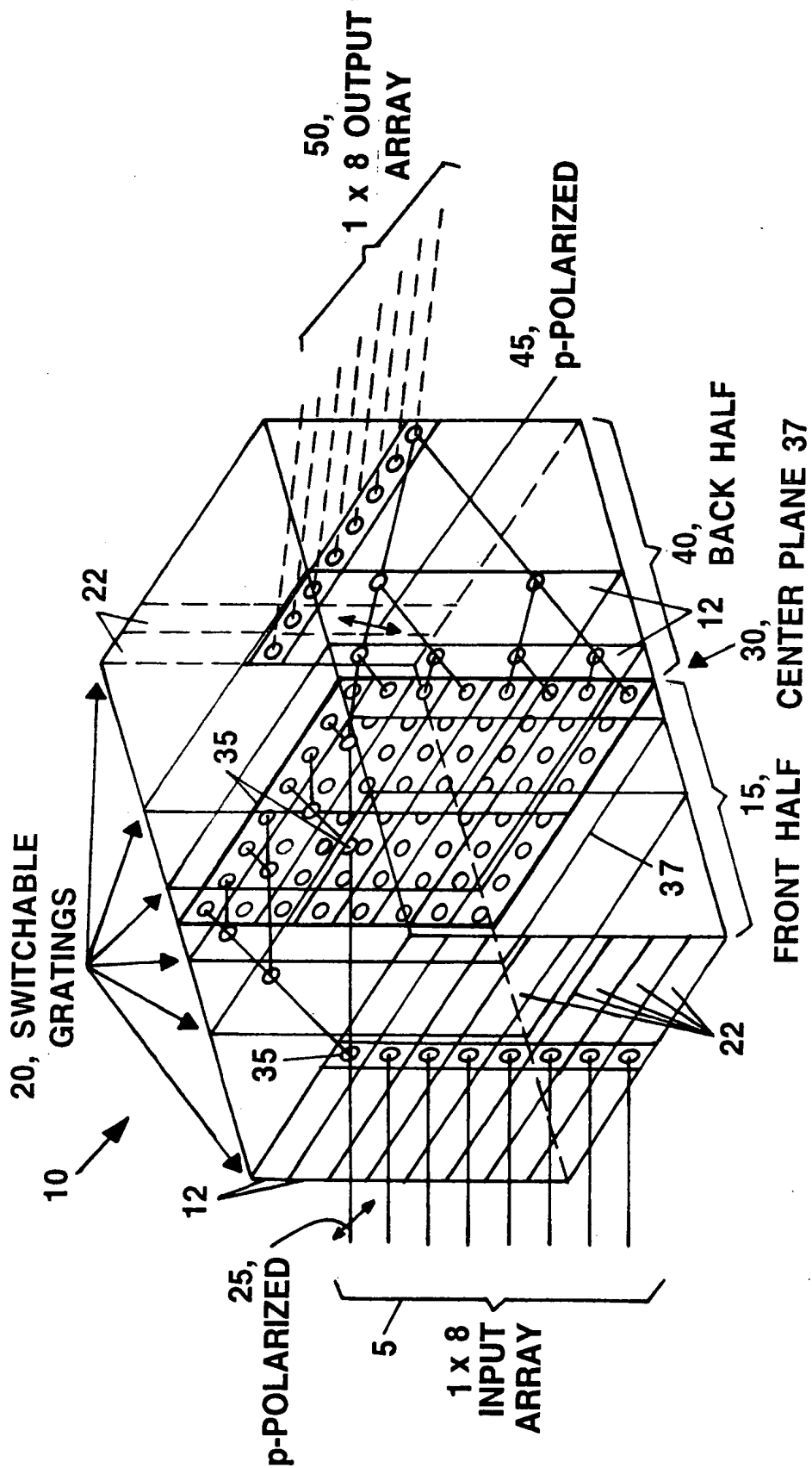


FIG. 1

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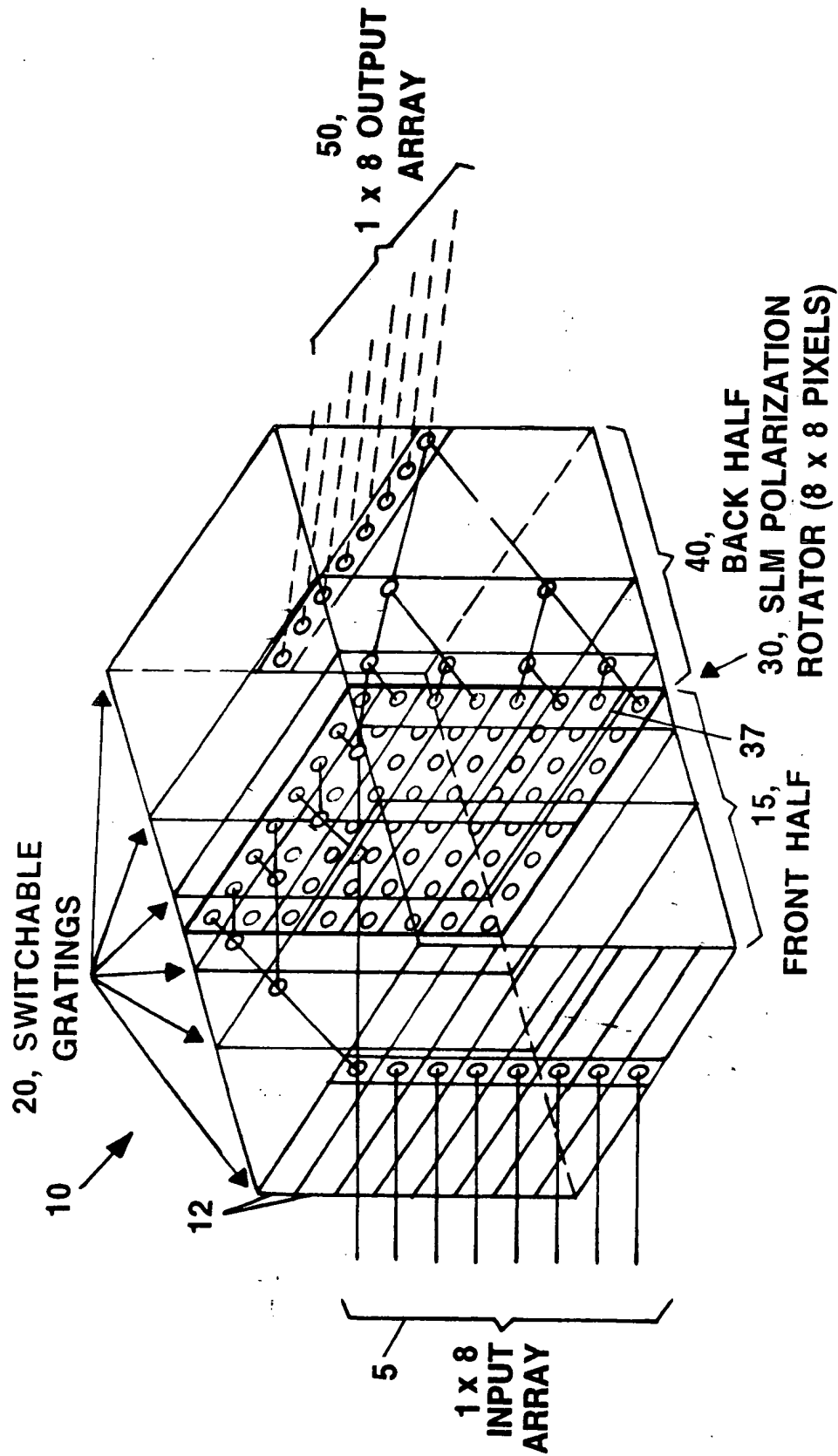


FIG. 2

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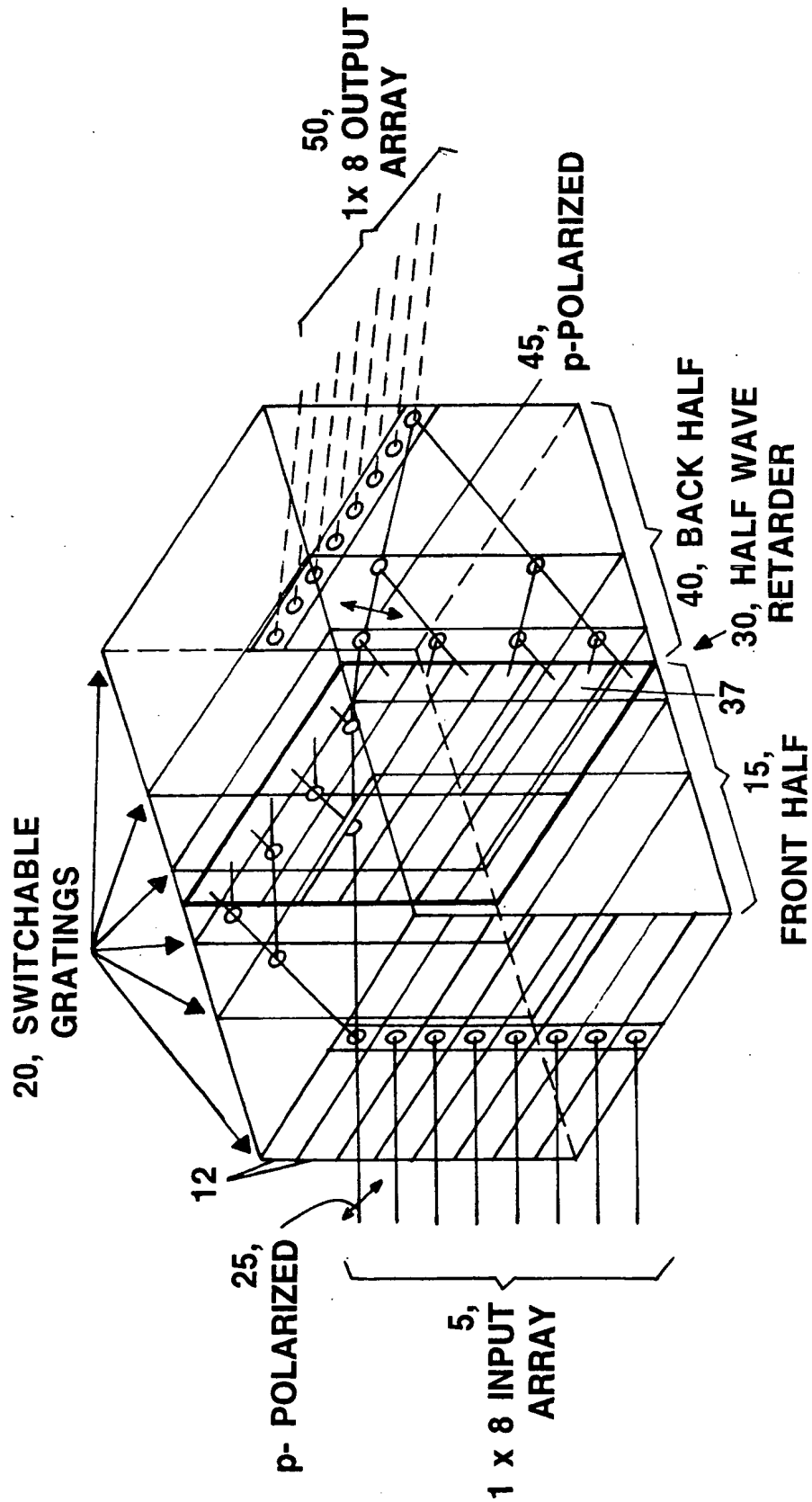


FIG. 3

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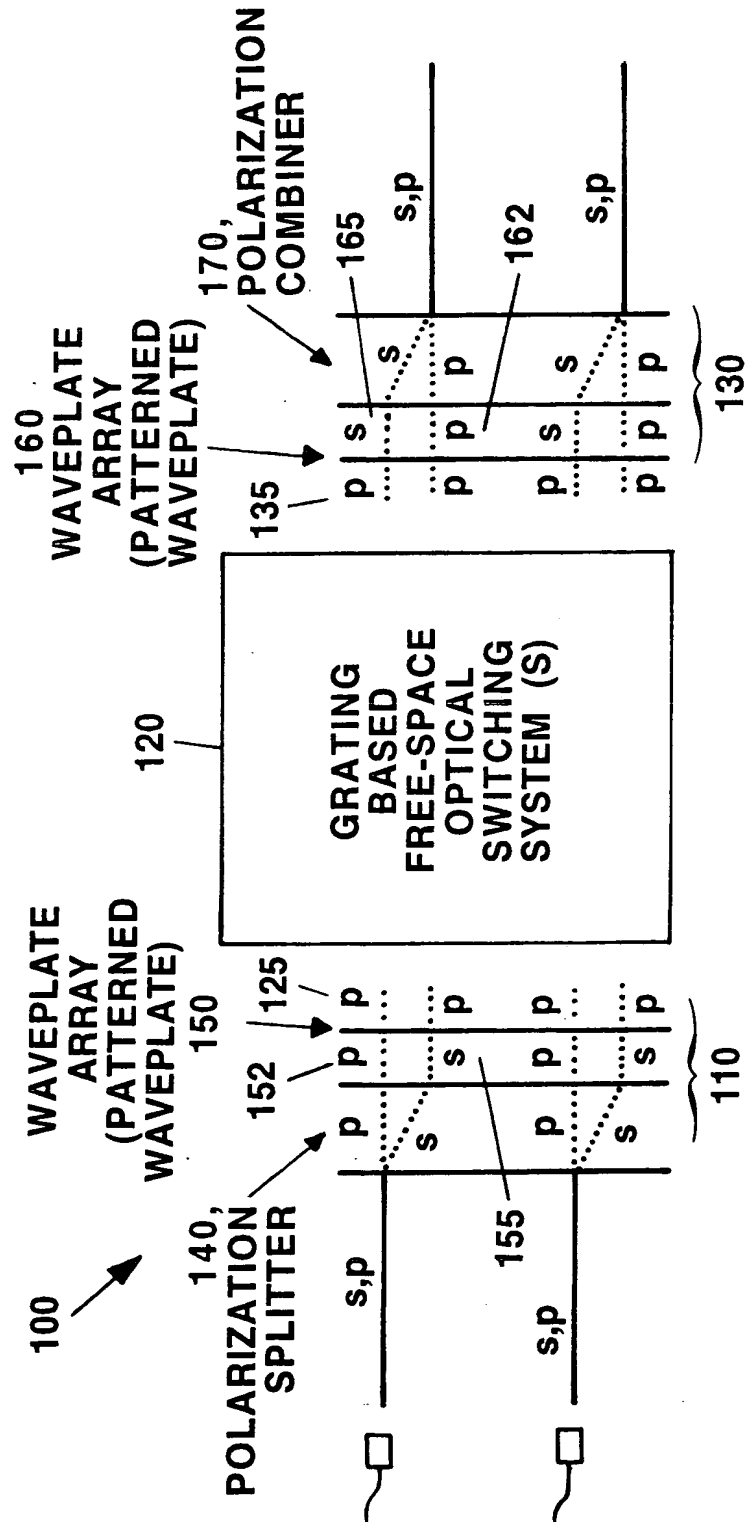


FIG. 4

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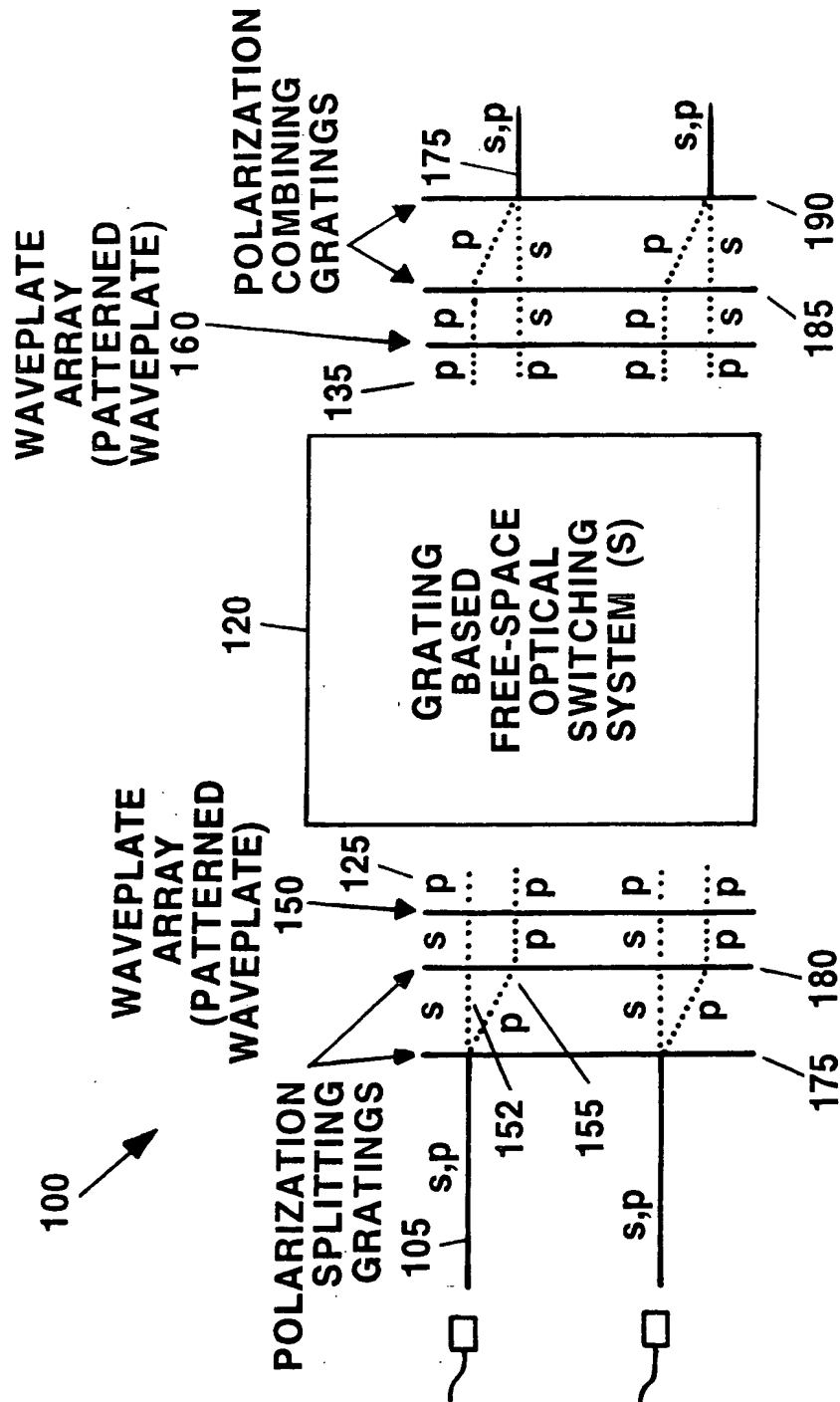
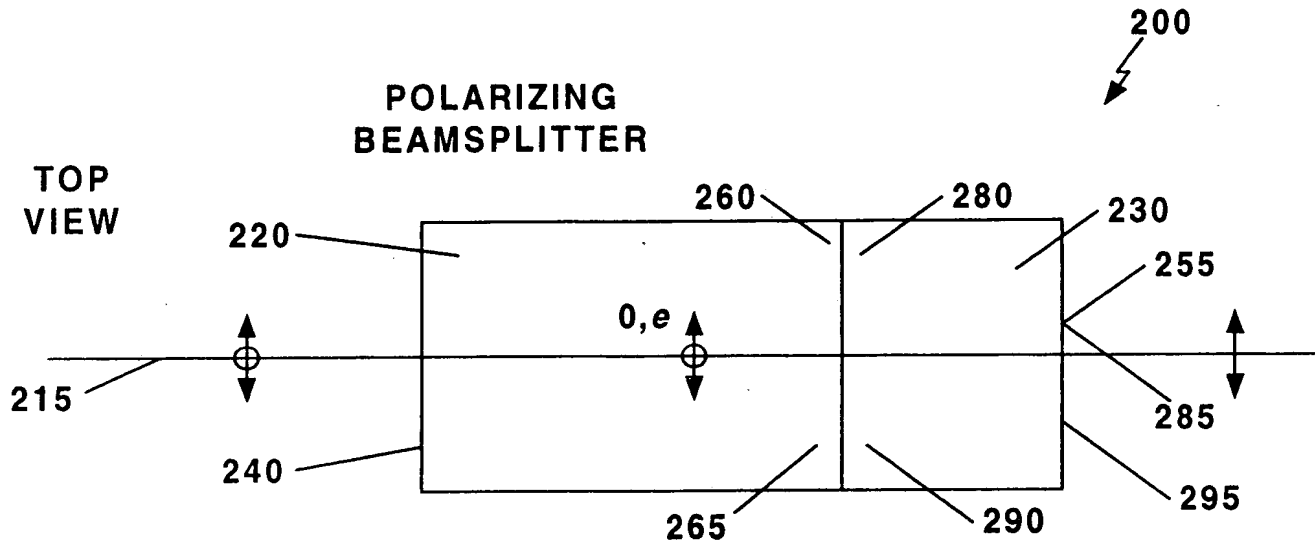


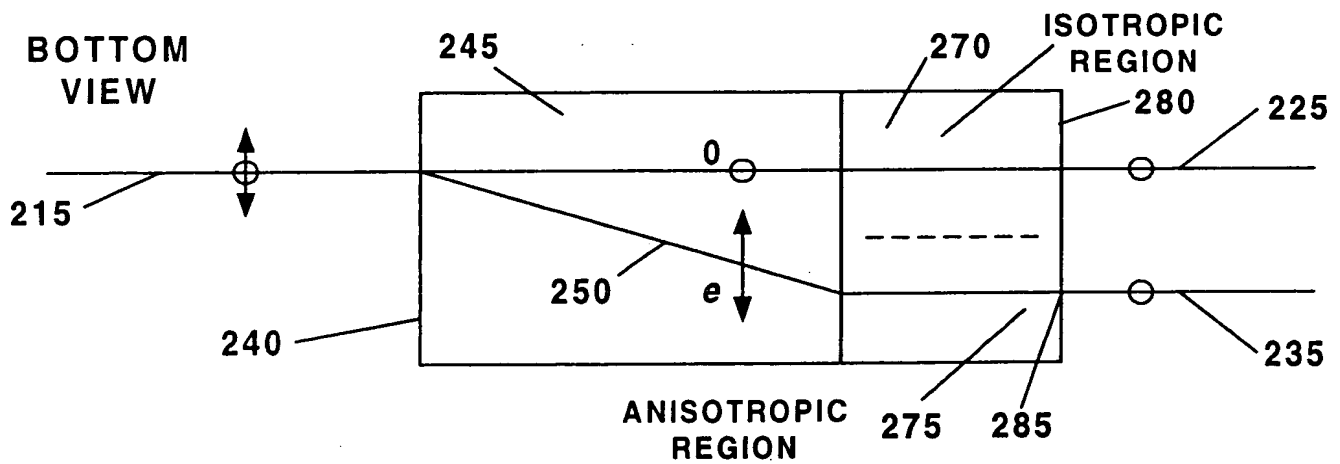
FIG. 5



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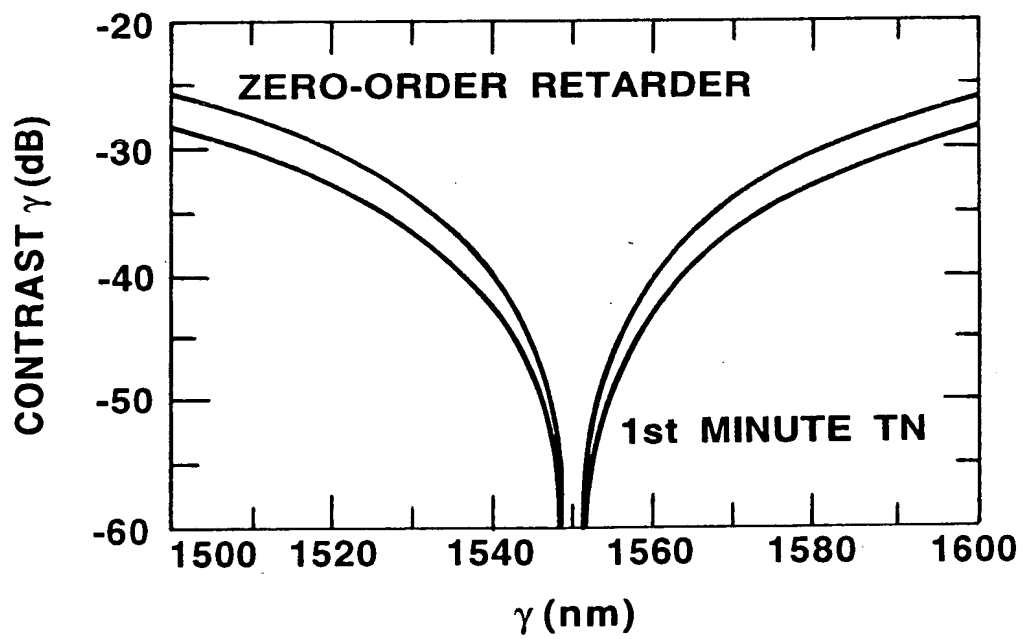
**FIG. 6A**



**FIG. 6B**

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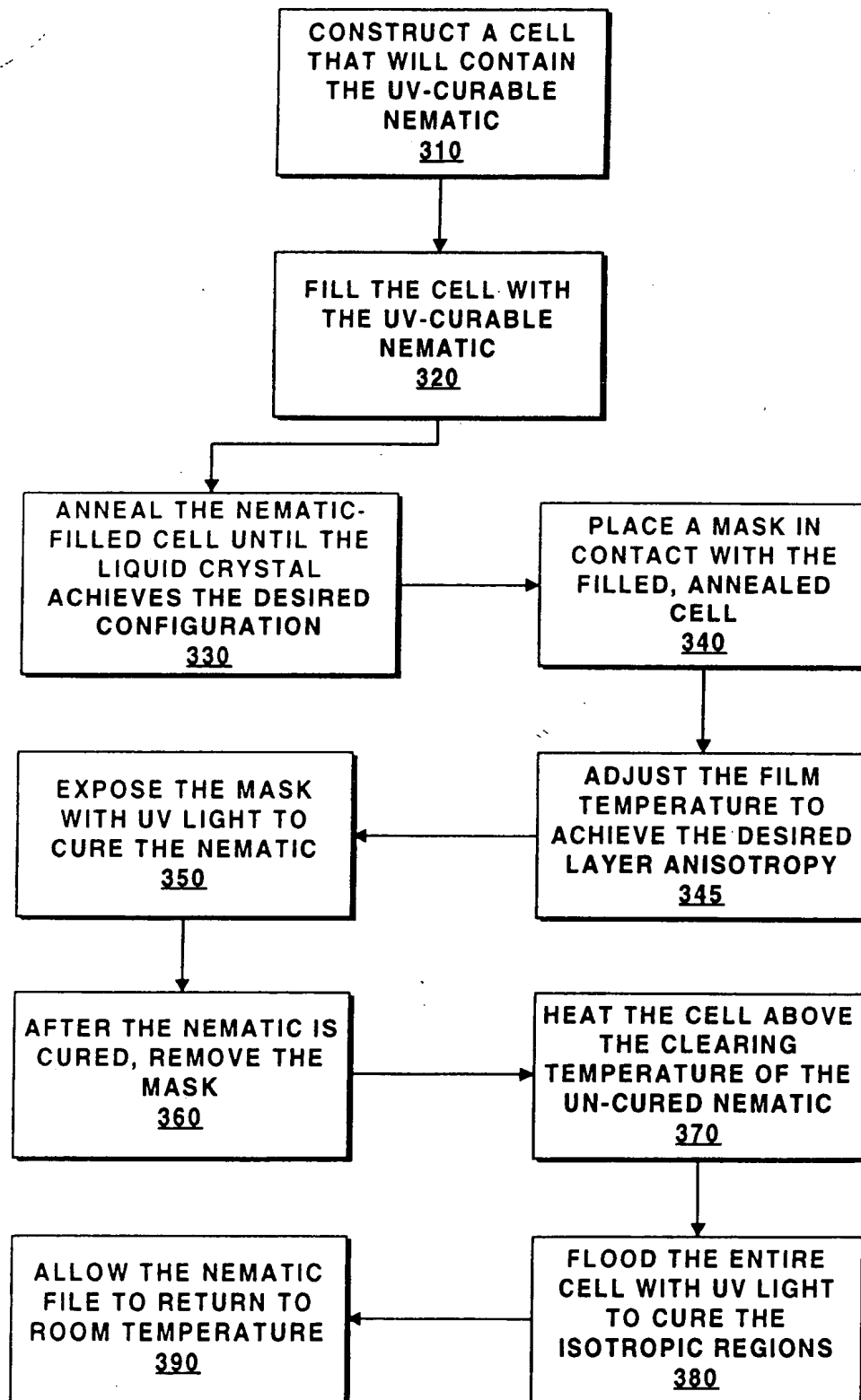
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**FIG. 7**

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**FIG. 8**

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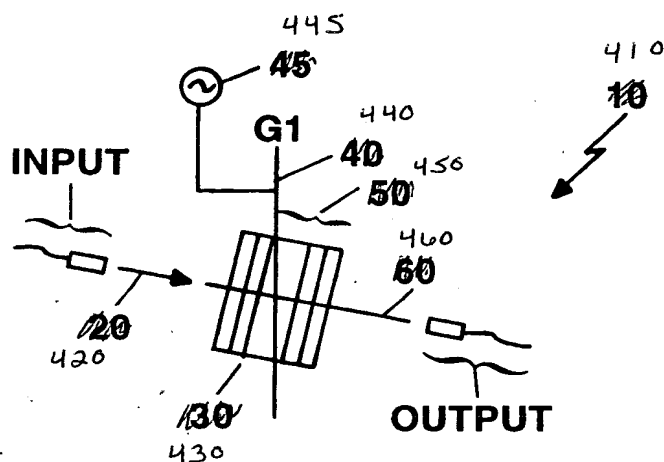


FIG. 1 9

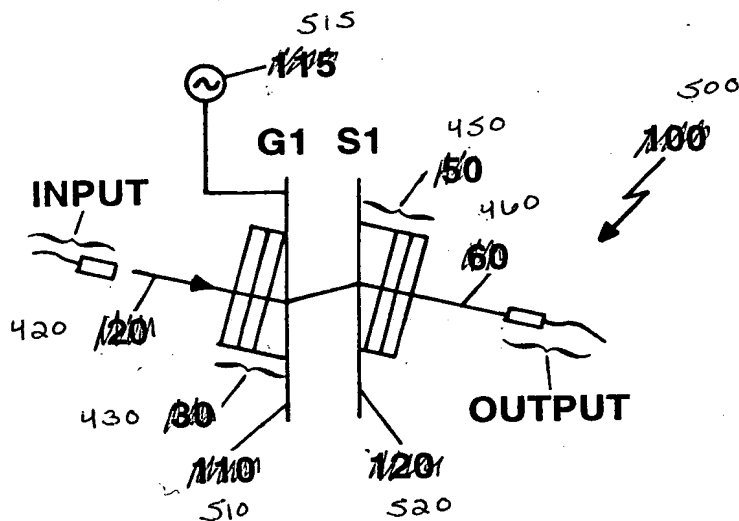


FIG. 2a 10a

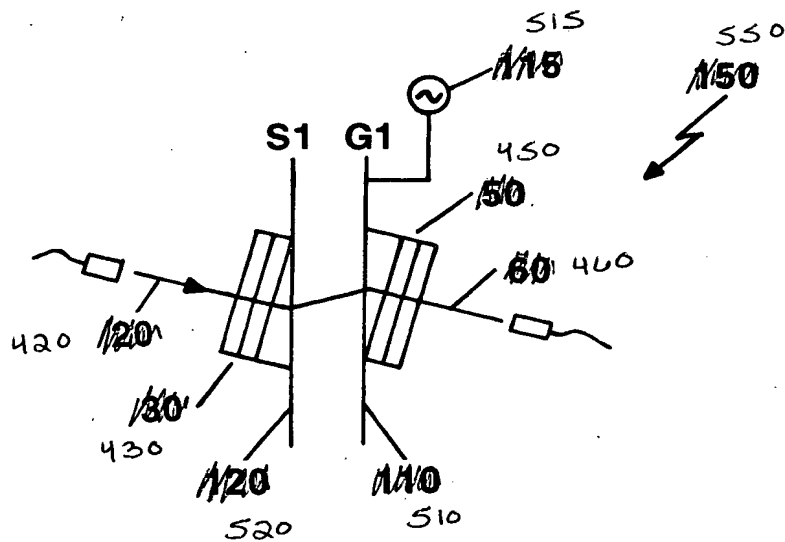


FIG. 2b 10b

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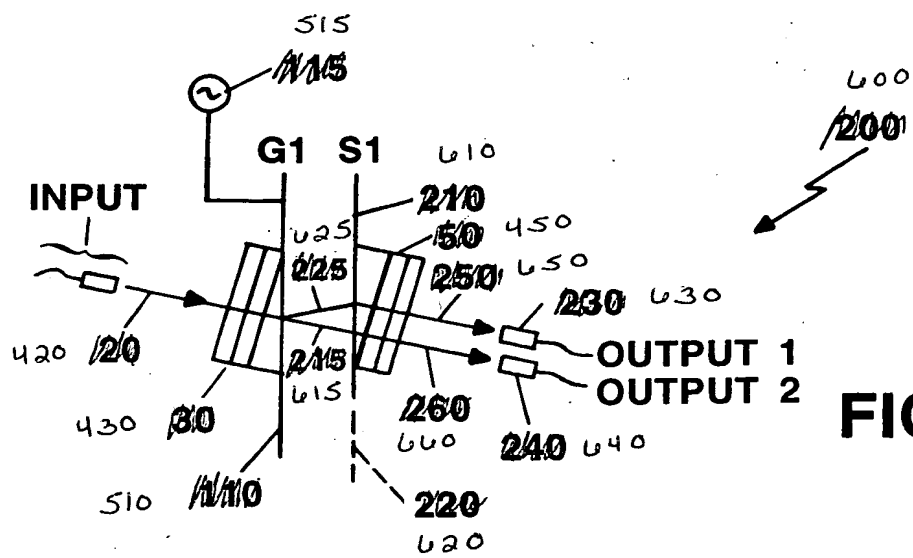


FIG. 3

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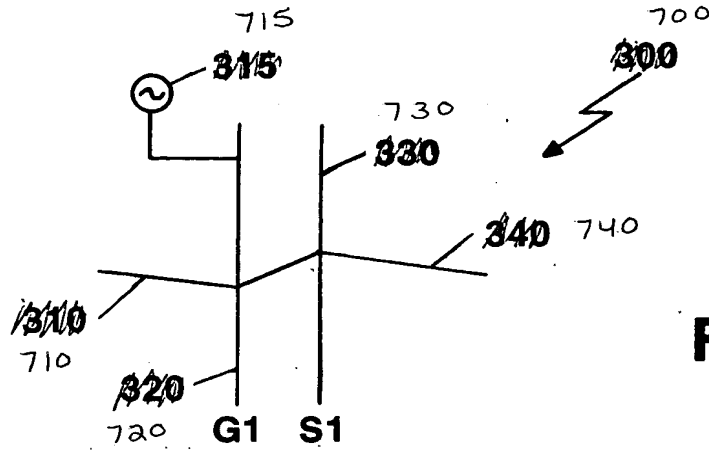


FIG. 4a 12a

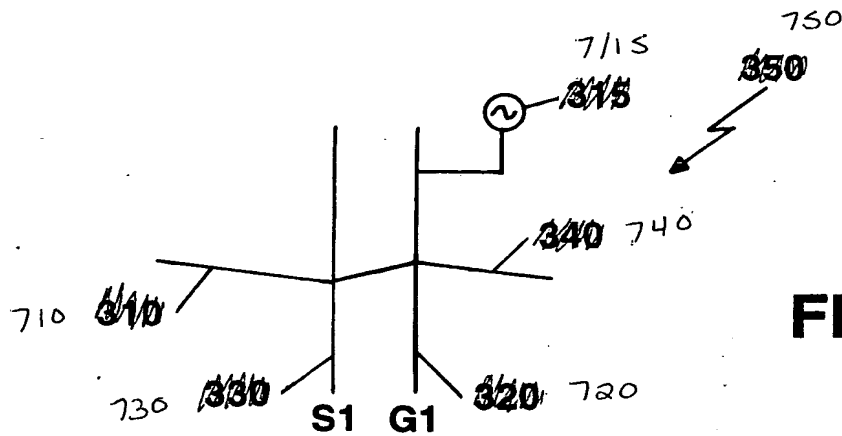


FIG. 4b 12b

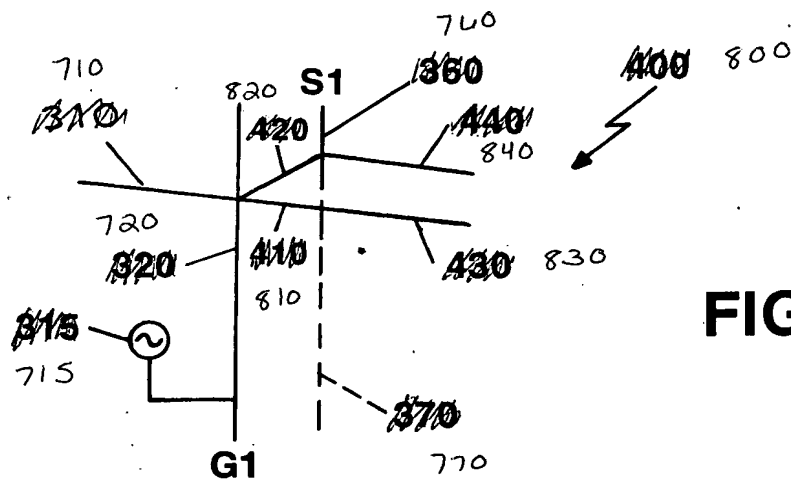


FIG. 5 13